

GPU-based algorithm for numerical simulation of CO₂ sorption

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Introduction

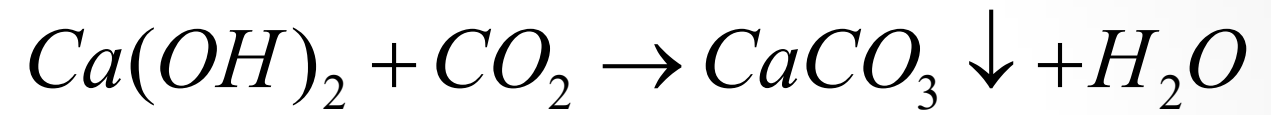


CO₂ chemisorption is widely used in

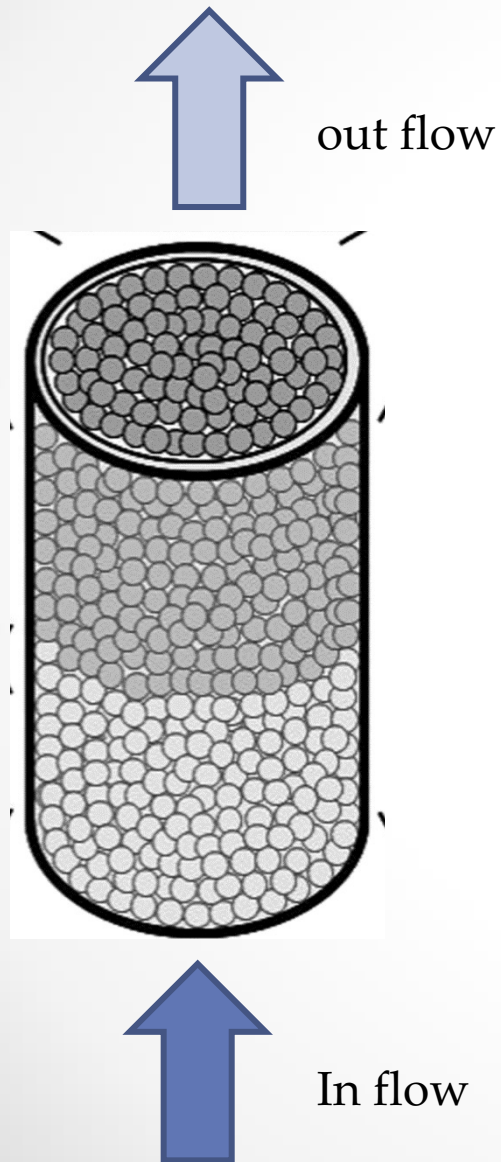
1. inhalation anesthesia
2. Respiratory care
3. hyperbaric chambers
4. underwater diving gear
5. fire safety apparatuses
6. mine rescue equipment.



Introduction



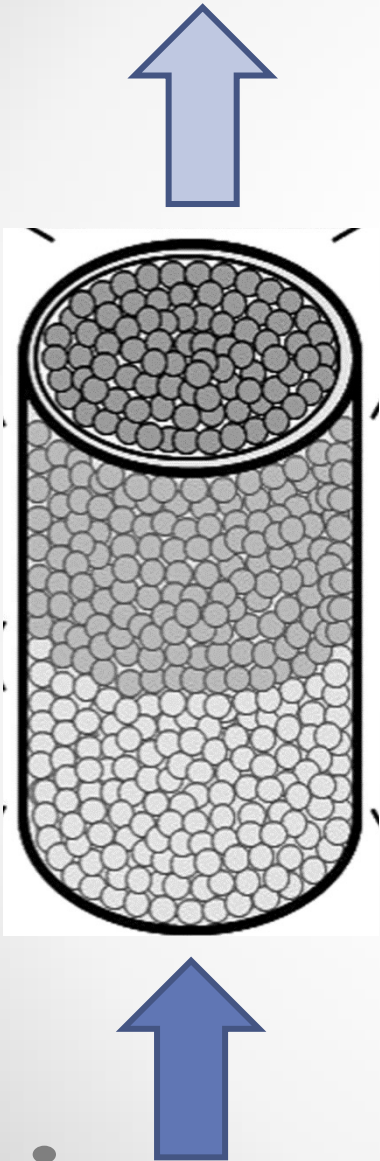
Introduction



Sorption efficiency depends on a number of physical parameters:

1. Pellets packing
2. Pellets shape
3. Internal porosity
4. Pore space structure
5. CO₂ concentration at inlet
6. Flow regime
7.

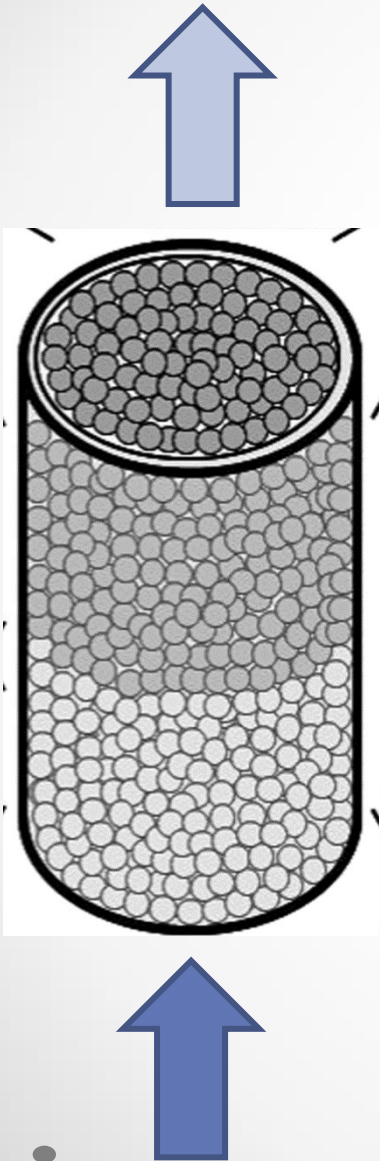
Mathematical model



Assumptions:

1. We deal with double-porosity model with large inter-particle pores and small-scale pores inside the particles
2. Only large-scale pores support the fluid flow
3. The only transport regime in the small-scale pores is the diffusion
4. The considered reaction is the first-order reaction

Mathematical model



Fluid flow

$$\nabla p - \mu \Delta u = 0$$

$$\nabla \cdot u = 0$$

$$x \in \Omega_F$$

Reactive transport

$$\frac{\partial \phi C_j}{\partial t} + \nabla \cdot (u C_j) - \nabla \cdot (D_j \nabla C_j) = F_j(C)$$

$$x \in \Omega_F \cup \Omega_G$$

Mathematical model

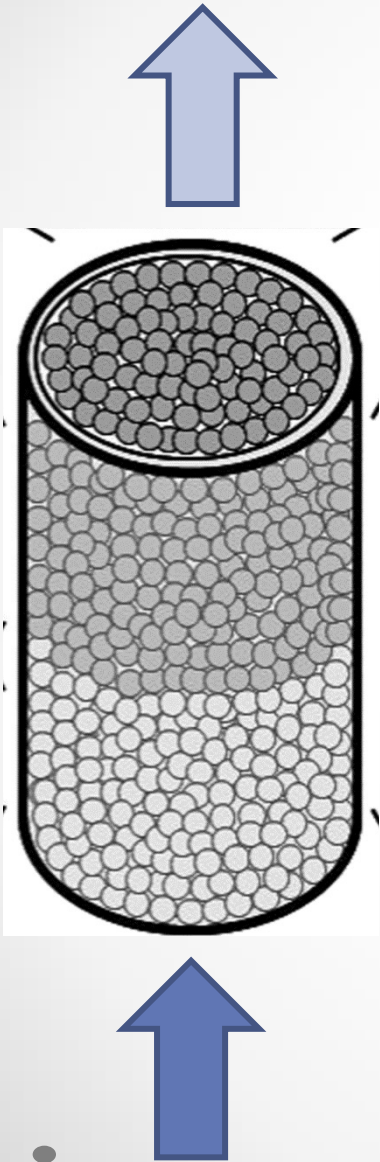
Reactive transport

$$\frac{\partial \phi C_{CO_2}}{\partial t} + \nabla \cdot (u C_{CO_2}) - \nabla \cdot (D_{CO_2} \nabla C_{CO_2}) = -k \phi C_{CO_2} C_{Ca(OH)_2},$$

$$\frac{\partial \phi C_{H_2O}}{\partial t} + \nabla \cdot (u C_{H_2O}) - \nabla \cdot (D_{H_2O} \nabla C_{H_2O}) = k \phi C_{CO_2} C_{Ca(OH)_2},$$

$$\frac{\partial C_{Ca(OH)_2}}{\partial t} = -k \phi C_{CO_2} C_{Ca(OH)_2},$$

$$\frac{\partial C_{CaCO_3}}{\partial t} = k \phi C_{CO_2} C_{Ca(OH)_2},$$

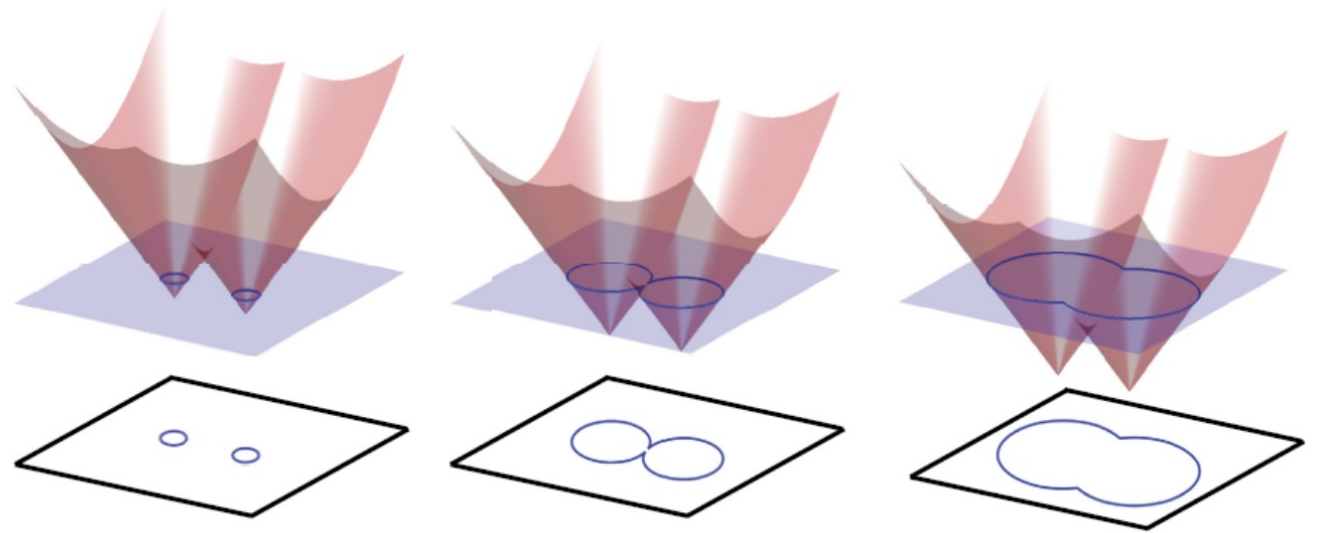
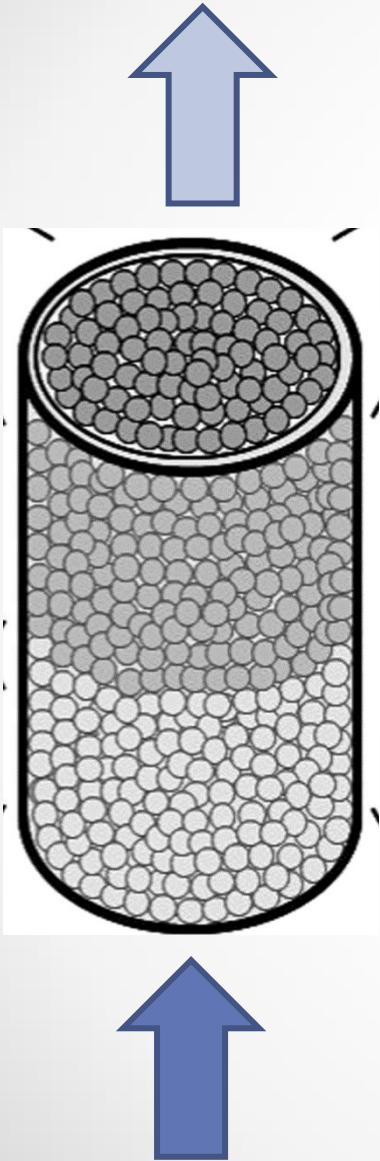


Numerical methods

1. Level-set to represent the model geometry

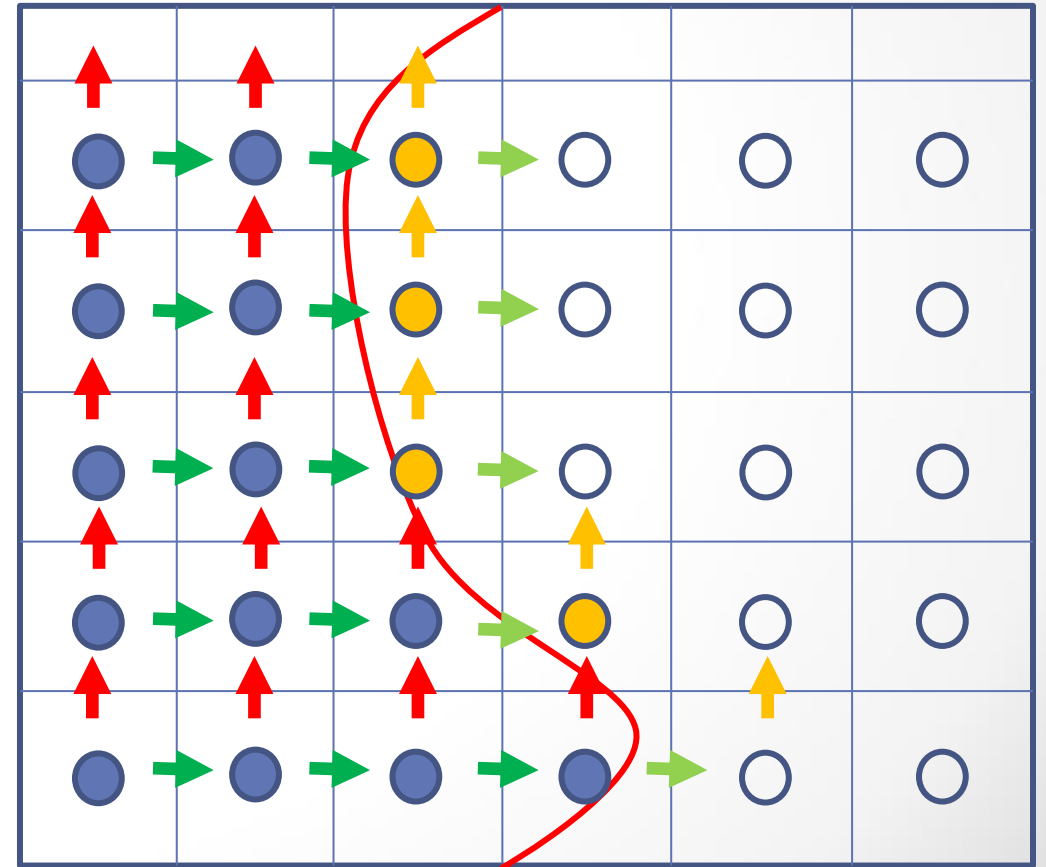
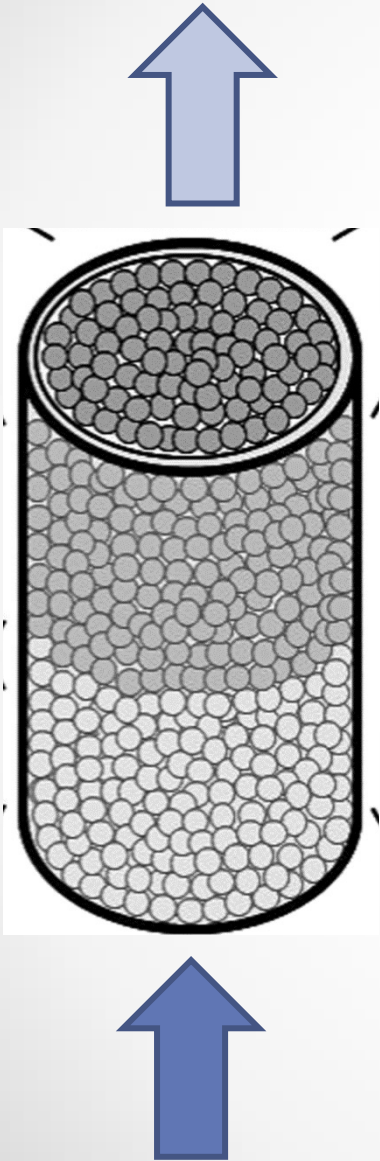
$$\Gamma(\vec{x}) = \{ \vec{x} \mid \varphi(\vec{x}, t) = 0 \},$$

$$\| \nabla_x \varphi(\vec{x}, t) \| = 1$$



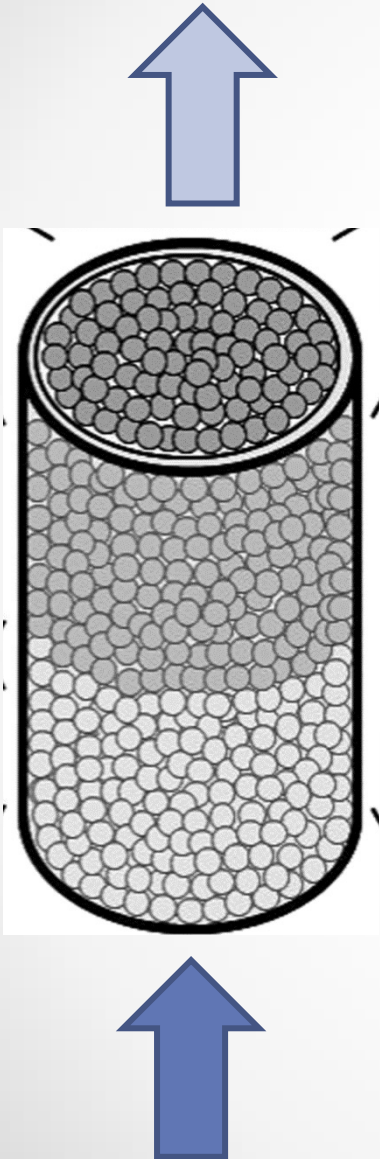
Numerical methods

1. Level-set to represent the model geometry
2. Immersed boundaries to account for irregular geometry



Numerical methods

1. Level-set to represent the model geometry
2. Immersed boundaries to account for irregular geometry
3. Projection-type method to solve Stokes equation with finite-difference approximation

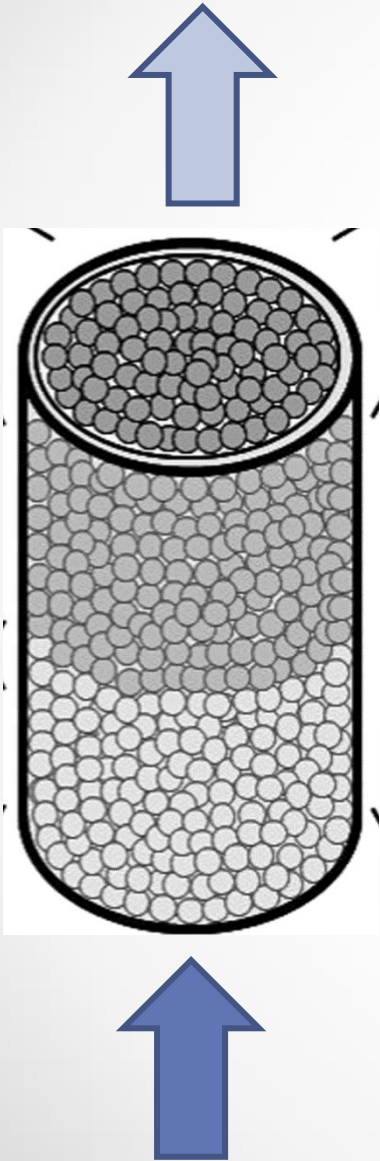


Numerical methods

1. Level-set to represent the model geometry
2. Immersed boundaries to account for irregular geometry
3. Projection-type method to solve Stokes equation with finite-difference approximation
4. AD+R splitting scheme to solve advection-diffusion reaction equation.
5. Explicit scheme for AD equation
6. Semi-implicit for R equation

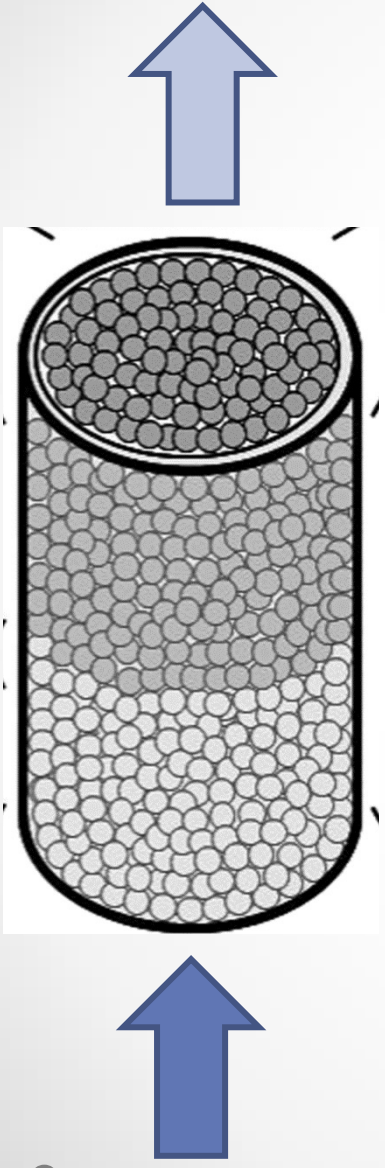
$$\phi \frac{C_j^{n+1/2} - C_j^n}{\tau} + \nabla_h \cdot (u C_j^n) - \nabla_h \cdot (D_j \nabla_h C_j^n) = 0$$

$$\frac{C_j^{n+1} - C_j^{n+1/2}}{\tau} = F_j(C_j^{n+1}, C_j^{n+1/2})$$



Numerical methods

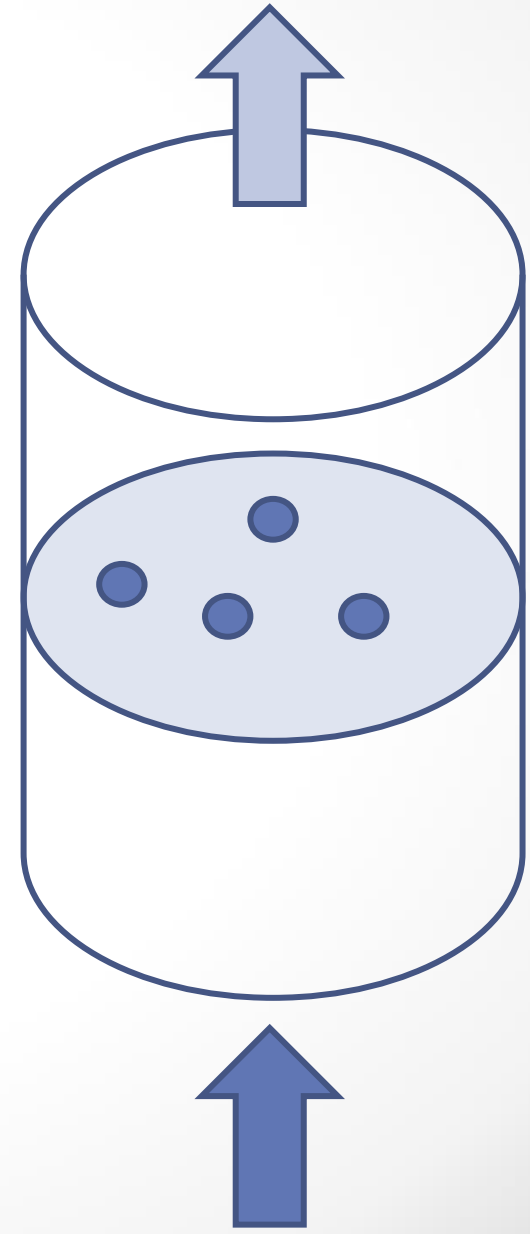
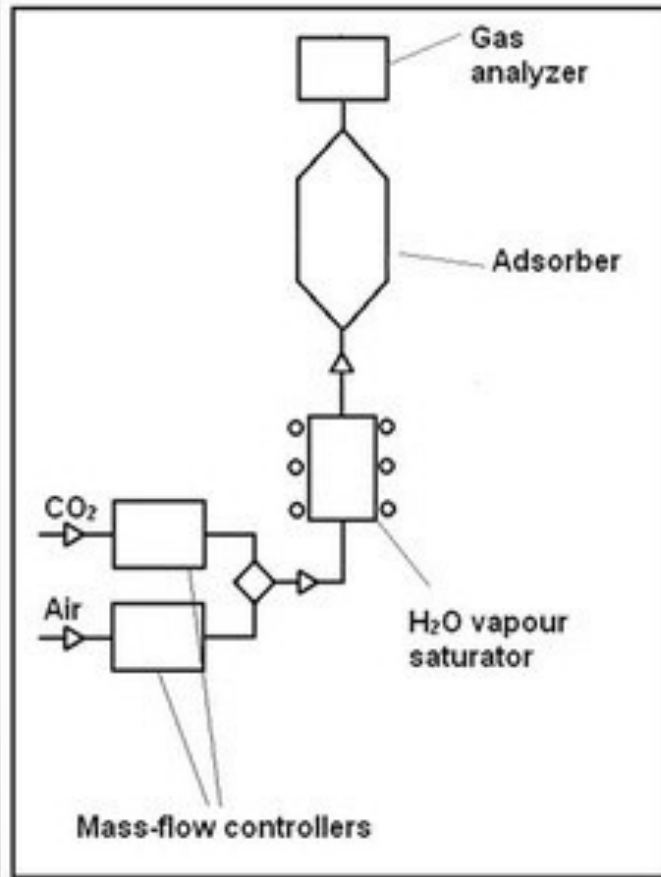
1. Level-set to represent the model geometry
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$$\frac{C_{CO_2}^{n+1} - C_{CO_2}^{n+1/2}}{\tau} = -k C_{CO_2}^{n+1} C_{Ca(OH)_2}^{n+1/2},$$

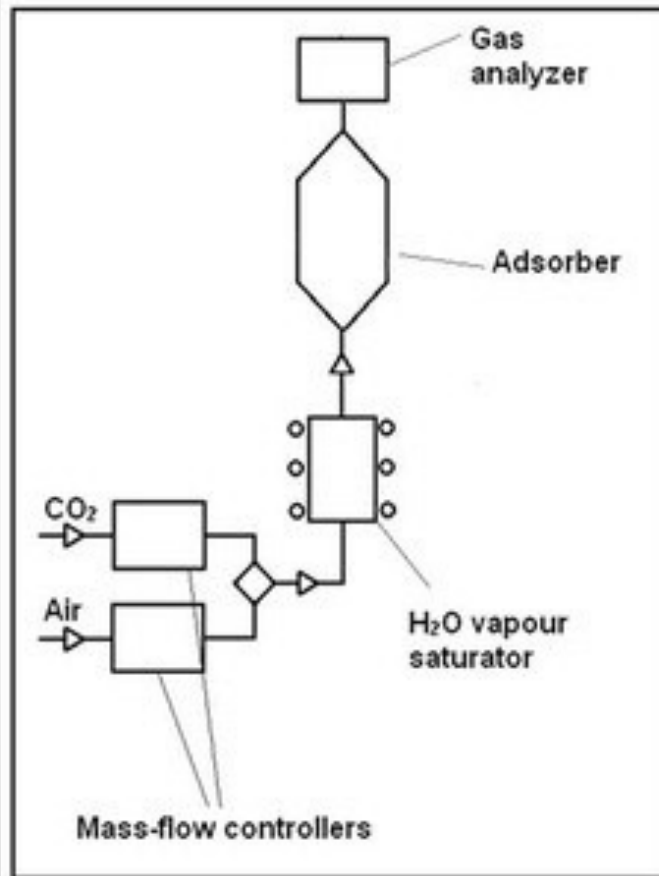
$$\frac{C_{Ca(OH)_2}^{n+1} - C_{Ca(OH)_2}^{n+1/2}}{\tau} = -\phi k C_{CO_2}^{n+1/2} C_{Ca(OH)_2}^{n+1},$$

$$\frac{C_{CaCO_3}^{n+1} - C_{CaCO_3}^{n+1/2}}{\tau} = -\phi k C_{CO_2}^{n+1} C_{Ca(OH)_2}^{n+1}.$$

Experiments



Experiments



<i>CO</i> ₂ concentration 5%				
	<i>t</i> = 0	<i>t</i> = 15	<i>t</i> = 30	<i>t</i> = 60
$\mu_{Ca(OH)_2}$	0.76	0.32	0.19	0.13
μ_{CaCO_3}	0.05	0.5	0.72	0.78
<i>CO</i> ₂ concentration 1%				
	<i>t</i> = 0	<i>t</i> = 15	<i>t</i> = 30	<i>t</i> = 60
$\mu_{Ca(OH)_2}$	0.6948	0.4604	0.3535	0.2672
μ_{CaCO_3}	0.0522	0.2318	0.3818	0.475

Numerical experiments

$$\frac{\partial \phi C_{CO_2}}{\partial t} + \nabla \cdot (u C_{CO_2}) - \nabla \cdot (D_{CO_2} \nabla C_{CO_2}) = -k \phi C_{CO_2} C_{Ca(OH)_2},$$

$$\frac{\partial C_{Ca(OH)_2}}{\partial t} = -k \phi C_{CO_2} C_{Ca(OH)_2},$$

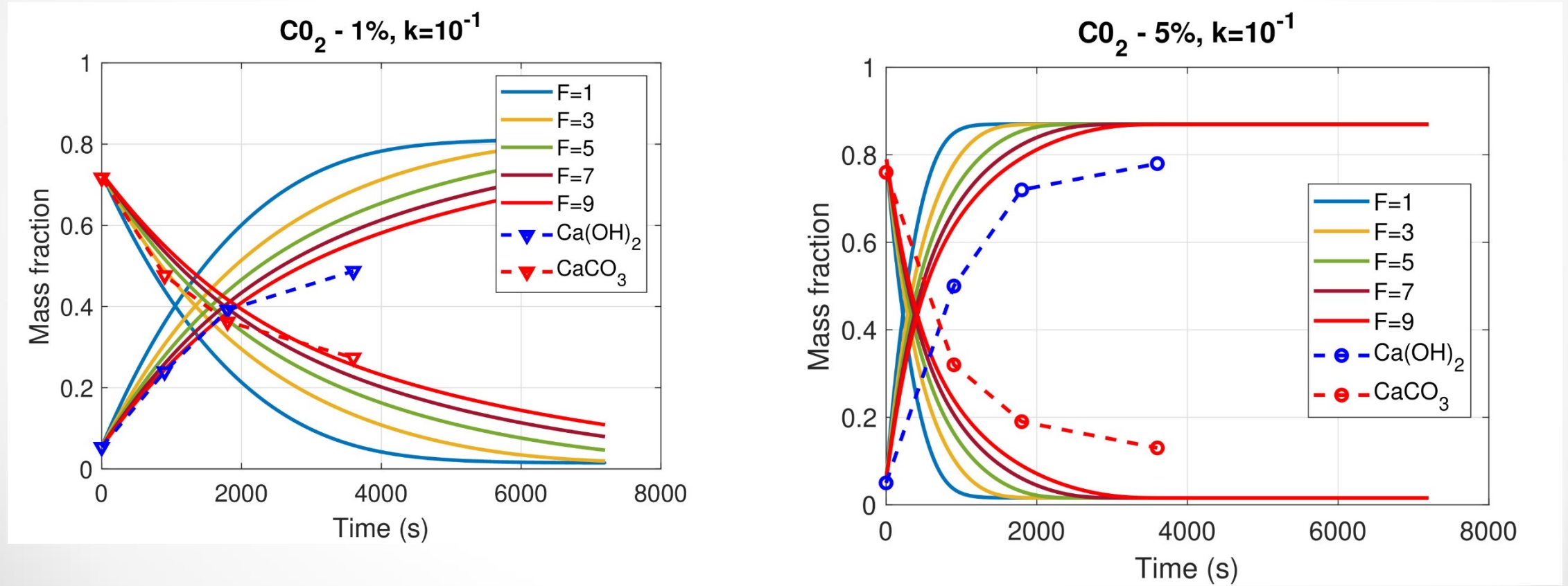
$$\frac{\partial C_{CaCO_3}}{\partial t} = k \phi C_{CO_2} C_{Ca(OH)_2}.$$

We do not know two parameters:

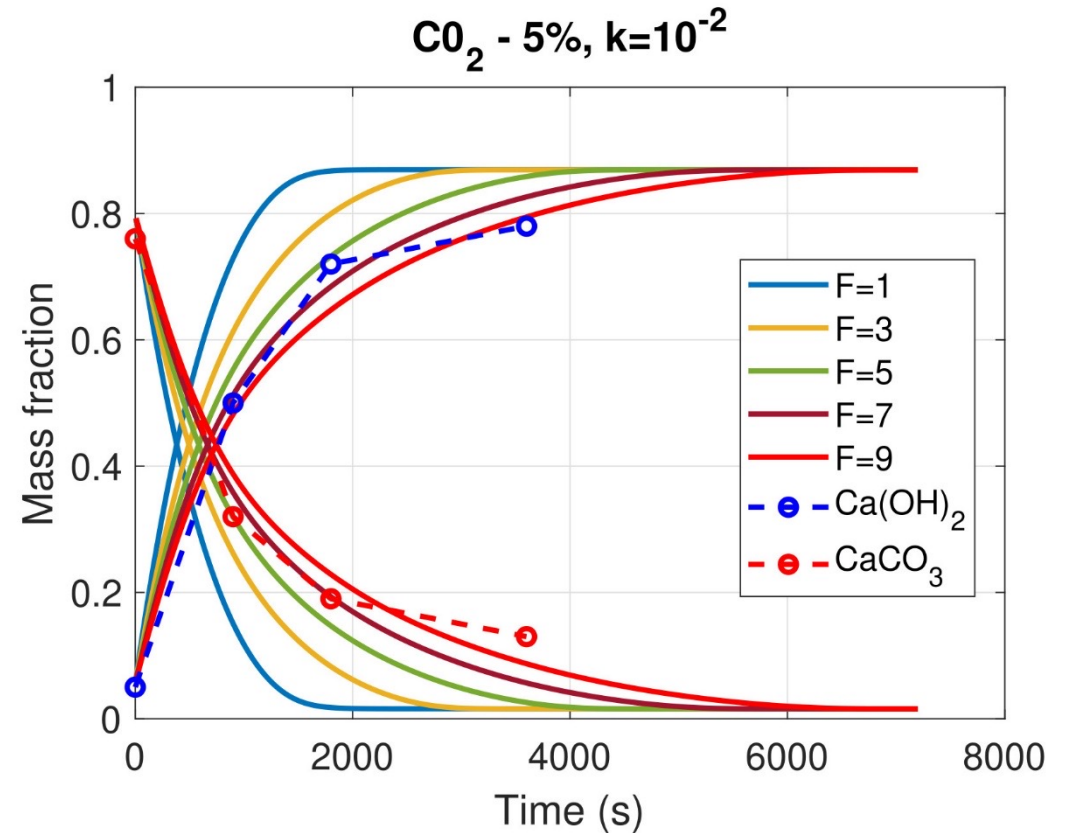
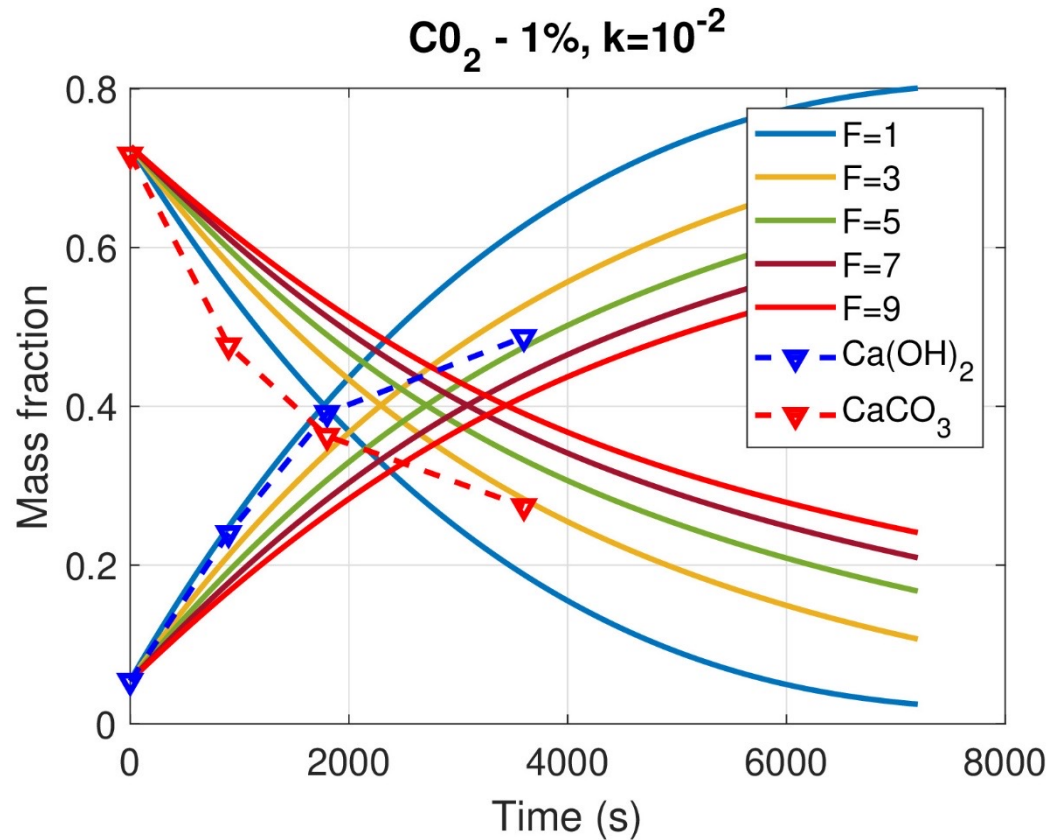
1. Reaction rate
2. Formation factor of the microporous space

$$D_{CO_2} = \frac{D_{CO_2}^0}{F}$$

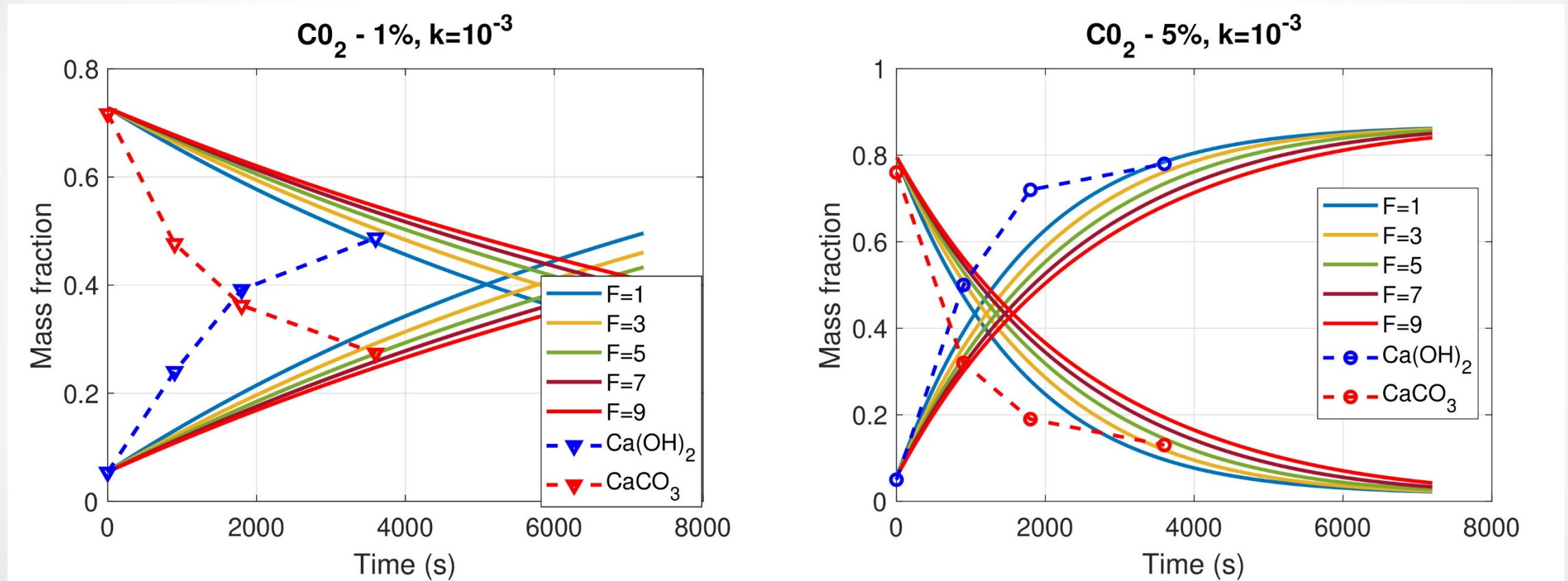
Numerical experiments



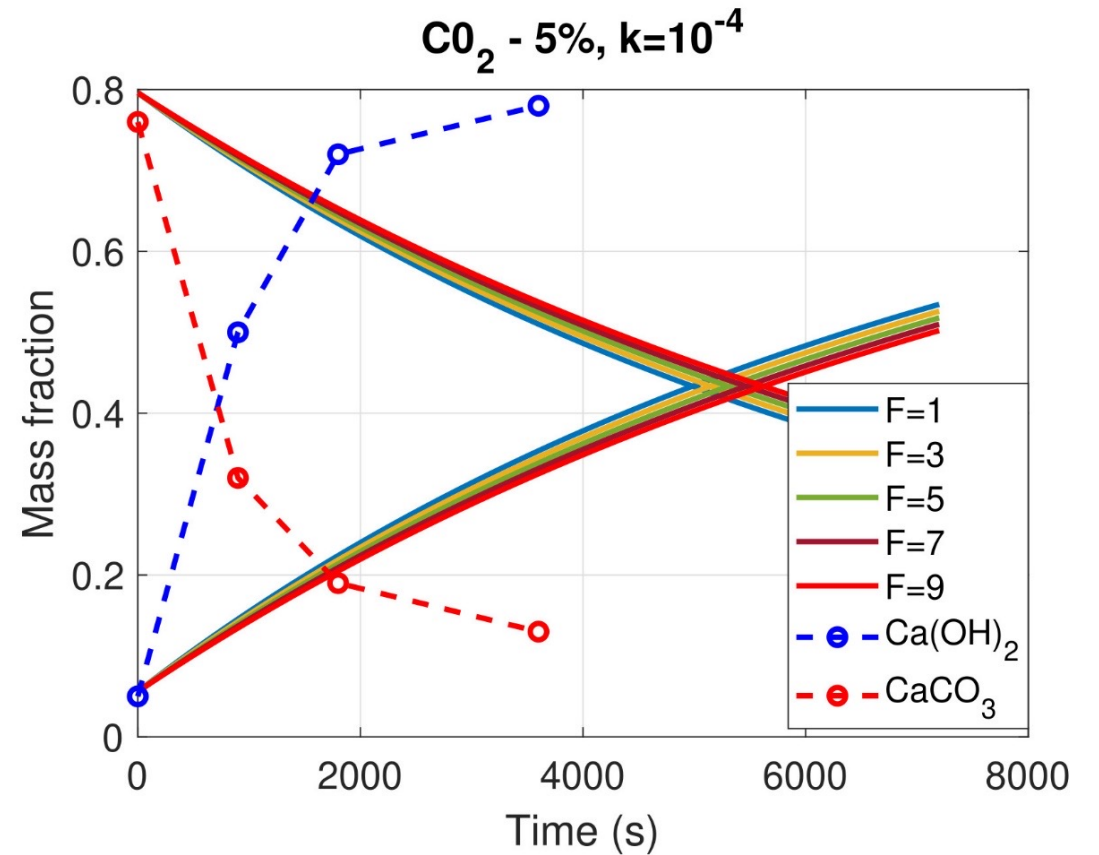
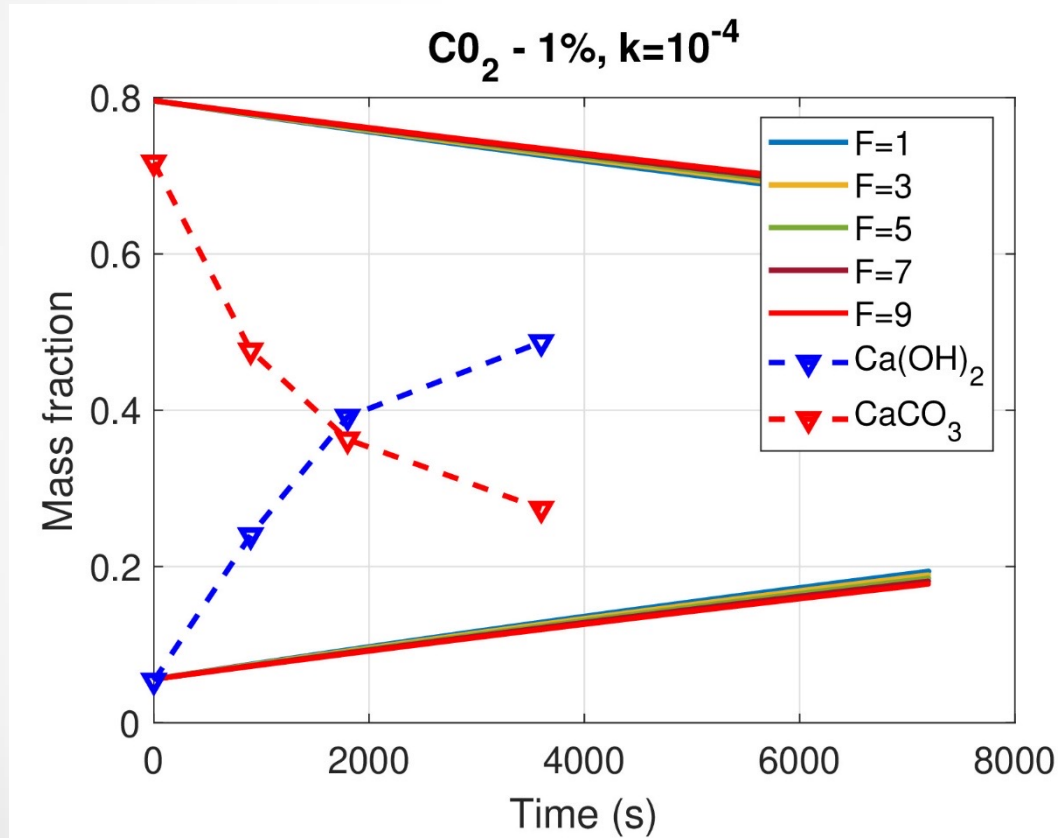
Numerical experiments



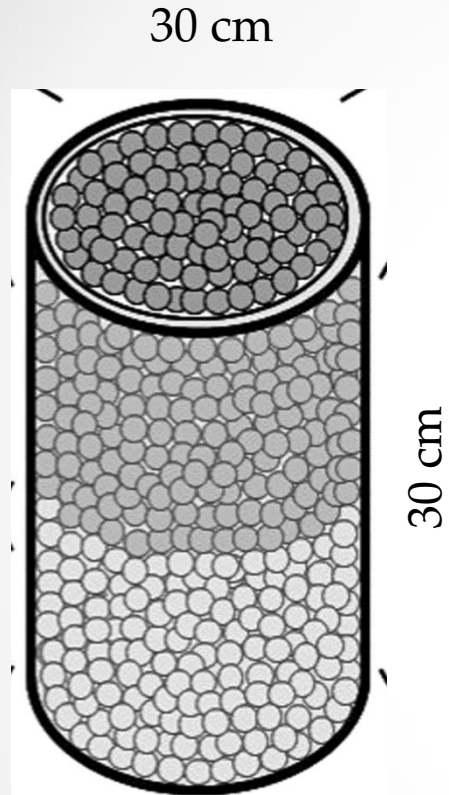
Numerical experiments



Numerical experiments



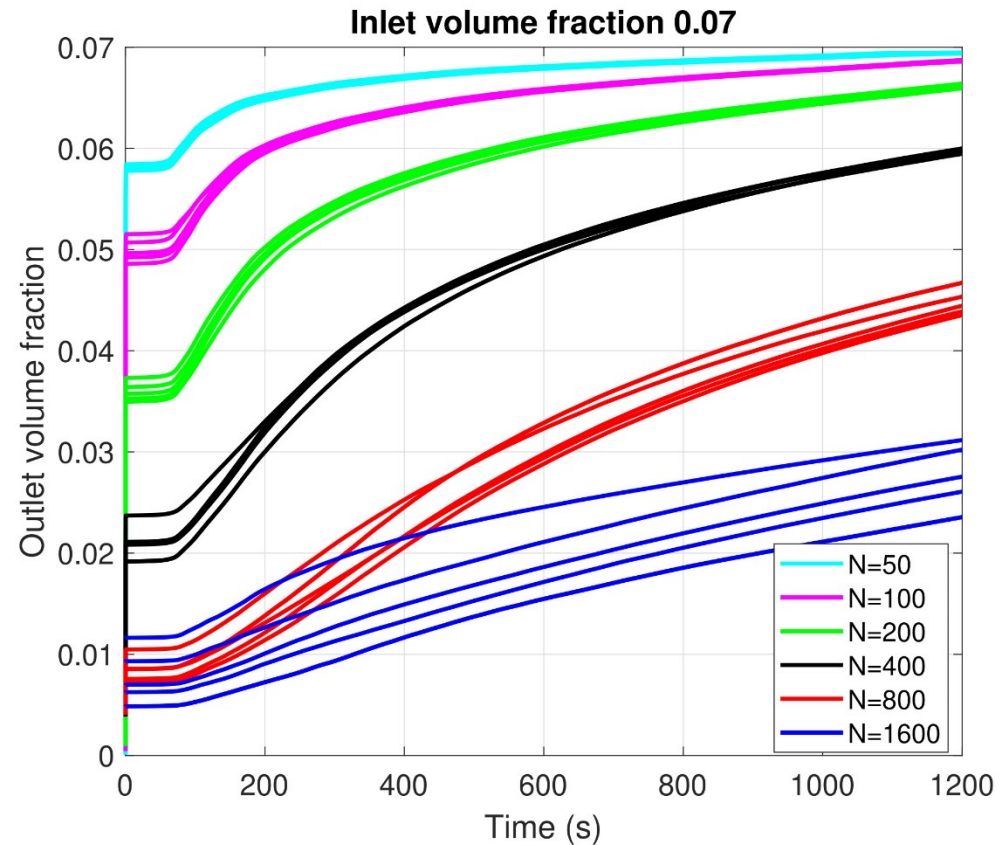
CO₂ break-through



Particle size 3 mm

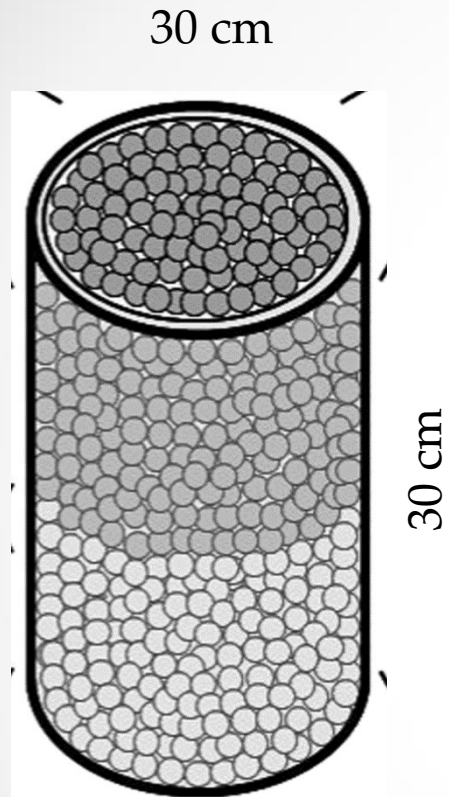
Number of particles 50, 100, 200, 400, 800, 1600

Grid step 0.3 mm



$$7.5 \cdot 10^{-5} \text{ m}^3 / \text{s}$$

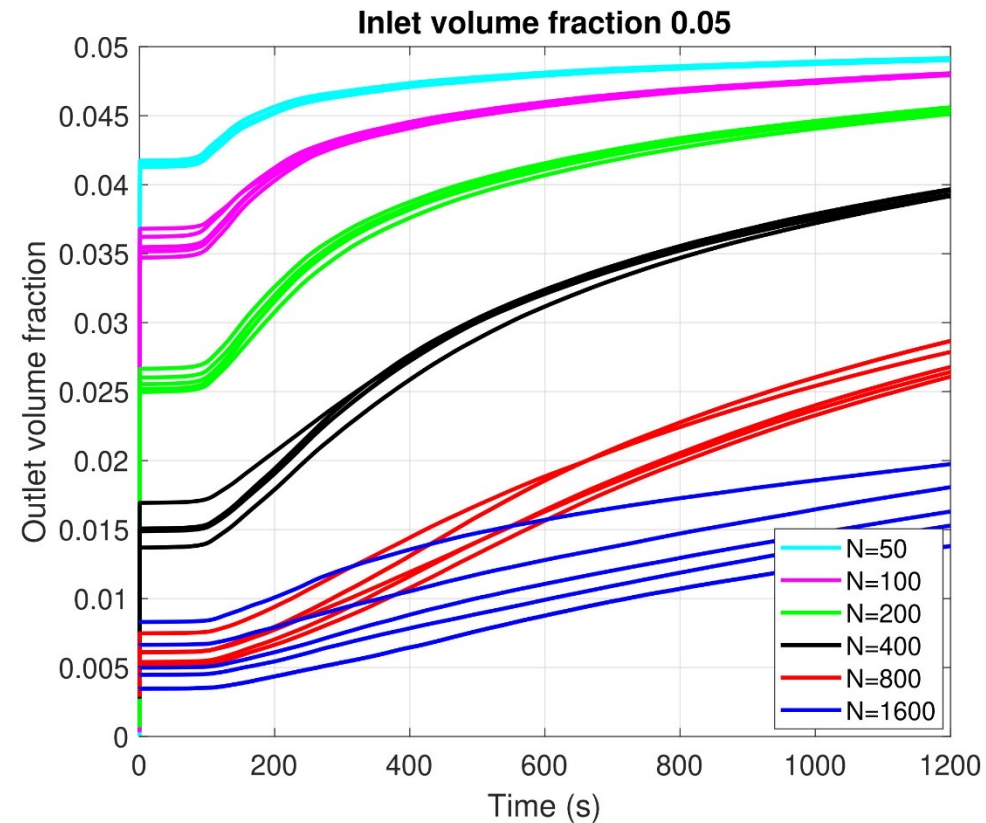
CO₂ break-through



Particle size 3 mm

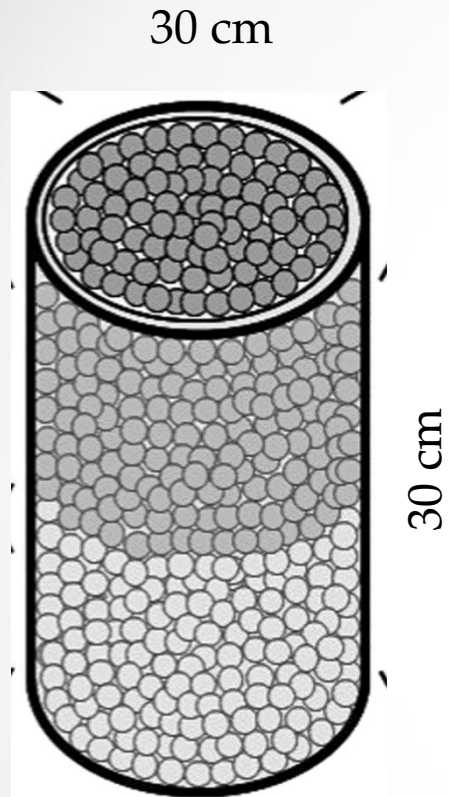
Number of particles 50, 100, 200, 400, 800, 1600

Grid step 0.3 mm



$$7.5 \cdot 10^{-5} \text{ m}^3 / \text{s}$$

CO2 break-through

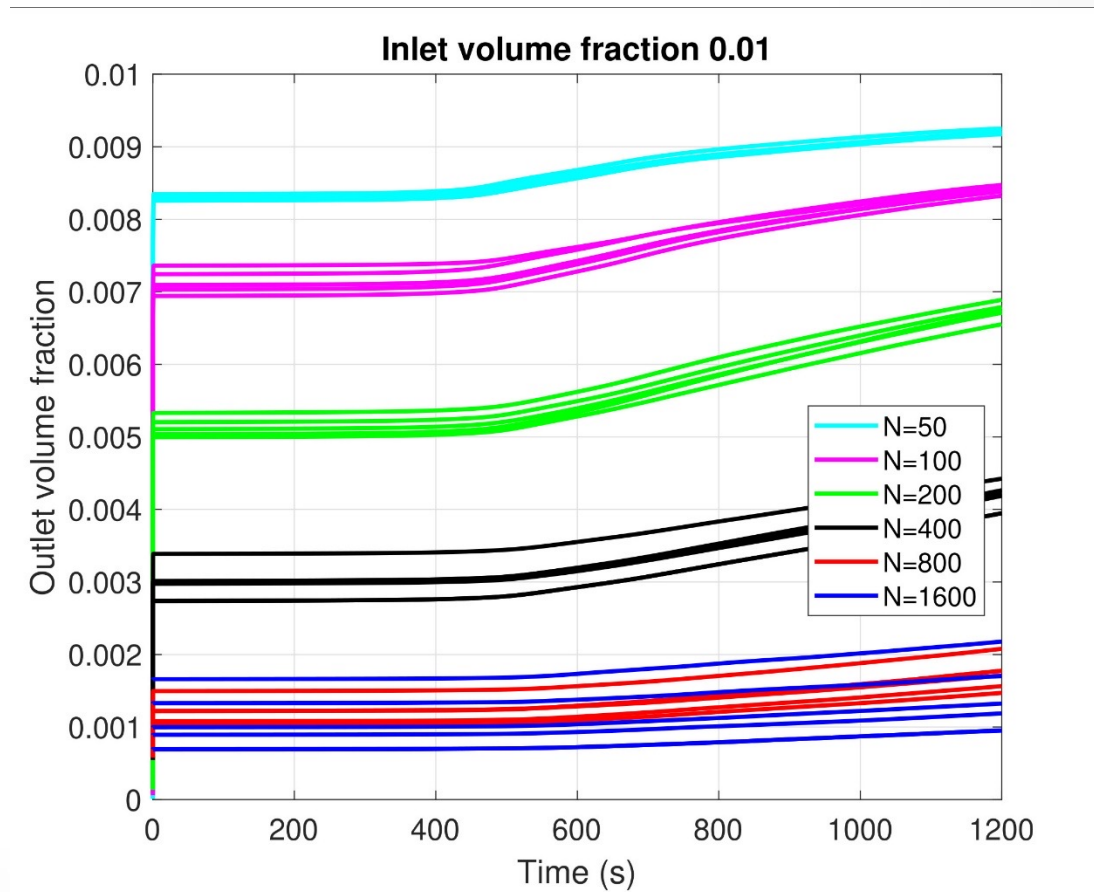


Particle size 3 mm

Number of particles 50, 100, 200, 400, 800, 1600

Grid step 0.3 mm

$$7.5 \cdot 10^{-5} \text{ m}^3 / \text{s}$$



Conclusions

1. We presented an algorithm for numerical simulation of CO₂ chemisorption.
2. The algorithm is implemented using CUDA technology and allows simulating real-size gas reactors using a single GPU.
3. We calibrate the unknown model parameters – reaction rate and the microporous space tortuosity to match the lab experiments.
4. We illustrate that the high density of sorbent particles packing increases the break-through time until the CO₂ diffusion rate starts limiting the reaction.

Thank you for attention!